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2 **SHAPE MEMORY ACTUATOR SYSTEM**

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4 The present invention relates in general to the displacement of an operational control  
5 element through an actuator cable having shape memory properties.

6 **BACKGROUND OF THE INVENTION**

7 The provision of additional operational control elements, such as control tabs installed at  
8 the trailing edge of the sternplanes on a submarine, has heretofore been considered in order to  
9 improve operational performance of the submarine with respect to sternplane jam recovery, and  
10 low and high speed maneuvering of the submarine. Such hydrodynamic control tabs are  
11 analogous to use of trim tabs on airfoils such as aircraft wings. However, use of such additional  
12 control tabs involved certain problems such as installational space requirements for the associated  
13 remote control actuator system, and generation of structural noise. The advantage in utilizing  
14 shape-memory cables made of Nitinol for size reduction of the remote control actuator system is  
15 well suited for a submarine environment because of its non-magnetic and corrosion resistance  
16 properties. Use of thermoelastic Nitinol introduces other problems because of the cooling and  
17 resetting properties of Nitinol cables. It is therefore an important object of the present invention  
18 to provide a shape-memory type of actuator system for remote control of control tabs or the like  
19 on structures such as submarines despite the problems associated therewith, without excessive  
20 expansion of required installational space or generation of electrical motor noise.

23 **SUMMARY OF THE INVENTION**

24 In accordance with the present invention, a pivotally mounted trailing-edge control tab on  
25 a hydrodynamic foil such as the sternplane of a submarine is remotely controlled through a  
26 superelastic type of Nitinol actuating cable which undergoes stretching or elongation during  
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1 pivotal displacement of the tab by a maximized amount in response to a displacing force  
2 transferred to the cable through linkage means in the form of a pivot bar lever pivotally mounted  
3 within the submarine or within the sternplane itself in spaced relation to the control tab being  
4 remotely controlled. When the superelastic cable is stretched by pivotal displacement of the tab,  
5 loading is transferred therefrom through the pivot bar lever to a thermoelastic cable within which  
6 the displacing force is generated. Such transfer of loading is interrupted and loading is  
7 maintained by locking of the pivot bar lever through a releasable locking mechanism in a position  
8 holding the superelastic actuating cable in its fully stretched condition. The thermoelastic cable is  
9 anchored to the submarine frame at one end opposite its end connected to the pivot bar lever.  
10 Between its ends such thermoelastic cable extends through a heat exchanger within which the  
11 cable is intermittently heated by electrical current conducted therethrough causing cable  
12 contraction for force generating purposes. The thermoelastic cable is cooled by water between  
13 intervals of heating to enable the aforesaid unloading action of the locking mechanism on the  
14 pivot bar lever. Release of the locking mechanism after cooling allows the cooled thermoelastic  
15 cable to stretch while also allowing the control tab to return to its neutral position from the  
16 position of maximum displacement during contraction of the actuating cable.  
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#### 19 BRIEF DESCRIPTION OF DRAWING FIGURES

20 A more complete appreciation of the invention and many of its attendant advantages will  
21 be readily appreciated as the same becomes better understood by reference to the following  
22 detailed description when considered in connection with the accompanying drawing wherein:  
23

24 FIG. 1 is a partial side elevation view of a submarine having a sternplane on which a  
25 trailing edge control tab is mounted for remote control in accordance with one embodiment of the  
26 invention;  
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1           FIG. 2 is an enlarged partial section view taken substantially through a plane indicated by  
2 section line 2-2 in FIG. 1 showing portions of the remote control actuator system of the present  
3 invention;

4           FIG. 3 is a schematic block diagram of the actuator system partially shown in FIG. 2;

5           FIG. 4 is a partial transverse section view of the thermoelastic cable of the actuator system  
6 taken substantially through a plane indicated by section line 4-4 in FIG. 2; and  
7

8           FIG. 5 is a graphical illustration of superelastic characteristics of the actuator cable  
9 associated with the actuator system shown in FIGS. 2 and 3.

#### 10                   DETAILED DESCRIPTION OF PREFERRED EMBODIMENT

11           Referring now to the drawing in detail, FIG. 1 illustrates a submarine 10 of a generally  
12 known construction, mounting a standard type of hydrodynamic sternplane arrangement 12  
13 through which depth change and depth maintenance of the submarine within seawater is  
14 controlled by pivotal displacement of the primary surface control element 16 at the trailing end of  
15 the sternplane stabilizer 14. Such control through the sternplane arrangement 12 is performed by  
16 a hydraulic system within the submarine. However, in accordance with the present invention an  
17 additional operational control element is introduced in the form of a pivotally displaceable trim  
18 control tab 18 installed at the trailing edge of the sternplane arrangement 12 so as to improve  
19 vessel performance with respect to sternplane jam recovery, low and high speed maneuvering and  
20 provide other benefits such as a reduction in structural noises and use of a smaller hydraulic  
21 control system. Such additional control involving pivotal displacement of the trim tab 18 about  
22 its pivot 22, is effected by a remote control system 24 as schematically shown in FIG. 2 and  
23 diagrammed in FIG. 3.  
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1       The remote control system 24 includes force transmitting linkage means in the form of a  
2 pivot bar lever 26 pivotally mounted within the submarine for displacement about a pivot axis  
3 fixed to the submarine hull at pivot point 28 as shown in FIG. 2. A tab actuating cable 30 made  
4 of superelastic wires is connected to one end of the pivot bar 26 and extends therefrom without  
5 directional change through the sternplane components into the tab 18 to a pulley 32 therein, from  
6 which the cable 30 undergoes directional change for attachment at an interior location 34 to the  
7 tab 18. The other end of the pivot bar 26 is connected to one end of a thermoelastic wire cable 36  
8 anchored at its other end to a fixed plate 38 within the submarine in spaced adjacency to a water  
9 cooling tank 44 as diagrammed in FIG. 3. The fixedly anchored cable 36 extends through an  
10 electrically operated heat exchanger 40 of a generally known type. Such heat exchanger 40 is  
11 connected to a programmed power supply 42 through which the cable 36 is controllably heated  
12 within the heat exchanger 40 and cooled by water from the tank 44 to which warmed water is  
13 returned from the heat exchanger.  
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16       FIG. 3 also diagrams a releasable mechanical locking mechanism 46 at the pivot point 28,  
17 operative to hold the pivot bar 26 in a position to which it is angularly displaced by cable 36  
18 while under the loading of actuating cable 30. The superelastic alloy wire material from which  
19 cable 30 is made, is such that it undergoes elongation up to 6% when stressed by a force up to  
20 100,000 lbs per square inch as reflected by curve 48 in FIG. 5 and contracts from such elongated  
21 state as reflected by curve 50. Degradation of elongation of cable 30 due to cyclic loading and  
22 unloading imposed through elongation and contraction of cable 36 is avoided. Such relationship  
23 of load elongation for cable 30 to operation of system 24 is made possible by the characteristic of  
24 the superelastic alloy of cable 30 and the mechanical locking of pivot bar 26 in the fully stretched  
25 condition of cable 30 to thereby unload the other cable 36.  
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1 Movement is controllably imparted to the control tab 18 through cable 30 by heating and  
2 cooling of the cable 36, made of thermoelastic wire such as Nitinol, requiring less than 30 Ksi to  
3 stretch while capable of exerting up to 100,000 lbs per square inch by contraction in response to  
4 electrical resistance (joule) heating within the heat exchanger 40. A tab displacement force of up  
5 to 8000 lbs generated by heat responsive phase transformation of cable 36, is transmitted through  
6 the pivot bar 26 to the cable 30 for pivotal displacement of the tab 18 through a maximum desired  
7 angle about its pivot 22. The foregoing shape-memory contracting action of cable 36 in the  
8 described installation involves about 4% elongation recovery, associated with cyclically  
9 controlled inflow and outflow of cooling water to the heat exchanger 40 of system 24.  
10

11 As hereinbefore indicated, the tab 18 is angularly displaced from its neutral position by  
12 heat induced contraction of cable 36 generating a tab displacing force applied through the pivot  
13 bar 26 to cable 30 so as to cause its elongation while transmitting the displacing force to the tab  
14 until the cable 30 is fully stretched, whereupon the pivot bar 26 is locked in position by  
15 mechanism 46 so as to hold cable 30 fully stretched and unload the cable 36. The locking  
16 mechanism 46 may then be selectively released so as to enable contraction of cable 30 due to its  
17 superelasticity as reflected by curve 50 in FIG. 5. The cable 36 is thereby stretched after being  
18 cooled, allowing the tab 18 to return to its neural position with the locking mechanism released.  
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21 As shown in FIG. 4, the cable 36 according to the illustrated embodiment includes a  
22 plurality of individual Nitinol wires 52 which are electrically interconnected in parallel within the  
23 heat exchanger 40 for simultaneous electrical heating of the cable above its transformation  
24 temperature of 100°C so as to generate a cable contraction stress of 60,000 lbs per square inch  
25 during its shape-memory transformation as aforementioned. A total cross-sectional area of 1/8  
26 square inch for the cable 36 necessary for such transformation action is formed by 45 wires 52  
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1 having 0.060 inch diameters. The non-magnetic, corrosion resistance properties of Nitinol from  
2 which the wires 52 are made are well suited to the cable usage hereinbefore described within the  
3 submarine environment. As to the cable 30, it is also formed from a plurality of wires made from  
4 pseudoelastic alloys having superelasticity properties. Such wires may be braided or twisted to  
5 provide the necessary flexibility within a 1/8 square inch cross-sectional area for the cable 30  
6 with which no thermal actuation is associated as in the case of cable 36. The cable 30 moves the  
7 tab 18 only after it undergoes a change in stress.  
8

9 FIG. 3 also diagrams a measuring device 54 at the end of pivot bar 26 to which the cable  
10 36 is attached, so as to measure pivot bar displacement and supply a measurement signal to an  
11 electronic circuit in the power supply 42 for adjustment thereof so as to achieve the desired  
12 intermittent contraction of the cable 36 by electrical heating within the heat exchanger 40. Such  
13 heating is accomplished by the adjusted supply of electrical current in parallel to the cable wires  
14 52 acting as resistors. Cooling of the cable 36, on the other hand, is achieved by its submergence  
15 with water maintained close to ambient temperature by intermittent circulation to and from the  
16 water tanks 44.  
17

18 The remote control system 24 hereinbefore described is effective to impart angular  
19 displacement to tab 18 in one direction from its neutral position. (downwardly as viewed in  
20 FIGS. 1 and 2). It is therefore contemplated that at least one additional control system similar to  
21 that of system 24 may be employed by attachment to the tab for pivotal displacement thereof  
22 from the neutral position in the opposite direction (upwardly).  
23

24 Obviously, other modifications and variations of the present invention may be possible in  
25 light of the foregoing teachings. It is therefore to be understood that  
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27 the invention may be practiced otherwise than as specifically described.  
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2 SHAPE MEMORY ACTUATOR SYSTEM

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4 ABSTRACT OF THE DISCLOSURE

5 A control tab on a submarine or the like is angularly displaced by a remote control  
6 actuator system featuring a pair of shape-memory cables consisting of a superelastic actuating  
7 cable connected to the control tab and a force generating thermoelastic cable anchored to the  
8 submarine frame. A force transmitting lever interconnects the cables and is selectively locked by  
9 a releasable locking mechanism in a position holding the actuating cable fully stretched with the  
10 control tab displaced a maximum amount from its neutral position by the displacing force  
11 generated in the thermoelastic cable in response to heating thereof by electric current conducted  
12 therethrough.  
13



**FIG. 1**

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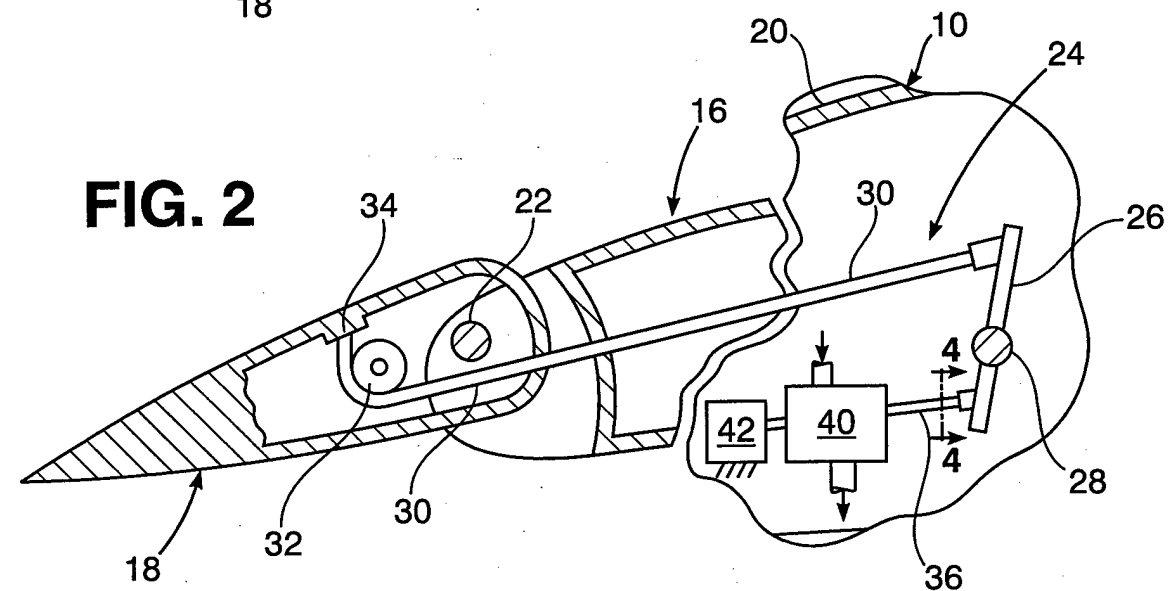
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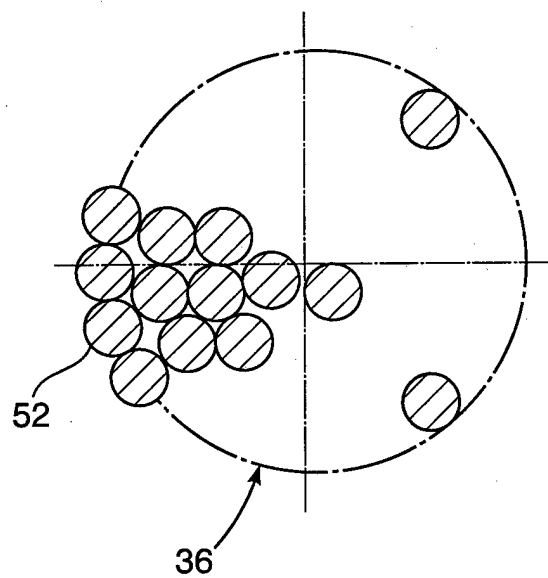
**FIG. 3**

The diagram illustrates a system for testing a releasable mechanical locking mechanism. The system components and their interconnections are as follows:

- PROGRAMMED POWER SUPPLY (42):** A rectangular block with a hatched input on the left. It is connected to the HEAT EXCHANGER (40) and the WATER TANKS (44).
- HEAT EXCHANGER (40):** A rectangular block that receives input from the PROGRAMMED POWER SUPPLY (42) and the WATER TANKS (44). It is connected to the WATER TANKS (44) and the RELEASABLE MECHANICAL LOCKING MECHANISM (24).
- WATER TANKS (44):** A rectangular block with a hatched input on the left. It receives input from the PROGRAMMED POWER SUPPLY (42) and the HEAT EXCHANGER (40). It is connected to the RELEASABLE MECHANICAL LOCKING MECHANISM (24).
- RELEASABLE MECHANICAL LOCKING MECHANISM (24):** A complex assembly consisting of:
  - 26:** A piston or plunger that moves vertically within a cylinder.
  - 30:** A seal or gasket that prevents leakage from the cylinder.
  - 36:** A rod or shaft that passes through the seal (30) and is connected to the piston (26).
  - 38:** A guide or support structure for the rod (36).
  - 54:** A component at the bottom of the rod (36), possibly a foot or a sensor.

The system is designed to test the locking mechanism by applying heat and pressure through the water tanks and heat exchanger.

**FIG. 4**



**FIG. 5**

